

## Deformation of Vesicles under the Influence of Strong Electric Fields II

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Dynamics of vesicle deformation in a pulsed electric field has been studied in the framework of perturbation theory. The membrane is assumed to be initially insulating and to become a conductor after a certain period of time,  $t_p$ , by electroporation. The dynamical behavior was found to be influenced not only by  $t_p$  but also by the ratio of the conductivity inside the vesicle and that outside.

**KEYWORDS:** vesicle deformation, dynamics, electroporation

### §1. Introduction

When a vesicle is subjected to a strong electric field, it often becomes porous, a phenomenon called electroporation.<sup>1,2)</sup> Thus, the membrane of the vesicle can be regarded as conducting medium. In an earlier report<sup>3)</sup> (called I hereafter), types of static deformation of vesicles having conducting membrane in static fields and dynamical behavior in pulse fields have been discussed. It was found that the deformation depends critically on the ratio of the conductivity inside the vesicle to that outside.

In I it was assumed that the electroporation occurs immediately after the field is turned on. However, in practice, the membrane may remain insulating for a significant period of time. If this is indeed the case, it is necessary to take into account the non-conducting membrane in order to describe the deformation dynamics of vesicles. Helfrich studied<sup>4-6)</sup> the shape of a spherical vesicle having insulating lipid bilayer, but his discussion did not include the dynamical behavior. In this report, we present the results of investigations of dynamics incorporating finite periods of insulating phase of membrane.

### §2. Formulation

#### 2.1 Electric fields and electric forces

Two fundamental equations determining electric fields are 1) the current conservation for a stationary state,  $\text{div } \mathbf{j} = 0$ , and 2) the ohm's law,  $\mathbf{j} = \sigma \mathbf{E}$ . These equations are solved under the following boundary conditions. The asymptotic form of the field at infinity is  $\mathbf{E} \rightarrow E_0 \hat{z}$ , where  $E_0$  is the field strength of the field applied in the  $z$ -direction. The boundary conditions on the membrane surfaces depend on whether the membrane is a conductor or an insulator.

If the membrane is an insulator, the normal component of the current at the vesicle surface must vanish. This leads to a condition that the field outside the vesicle,  $E_e$ , has no normal component,  $E_{en} = 0$ , at the surface. The field is determined uniquely by this condition.

The case of a conducting membrane has been discussed in I. It is necessary to consider the field inside the vesicle,  $E_i$ , as well as  $E_e$ . The boundary condition for the tangential component of the field is given as  $E_{it} = E_{et}$  and that

for the normal component is  $\sigma_i E_{in} = \sigma_e E_{en}$ .\*

The electric force exerted on the vesicle surface may be calculated from the Maxwell tensor, and the normal component is

$$F_n = -\frac{\epsilon_e}{8\pi} (E_{et})^2 \quad (1)$$

for an insulating membrane, where  $\epsilon_e$  is the dielectric constant of the outside medium.

#### 2.2 Small deformation from a spherical vesicle

The shape of a vesicle is represented in the polar coordinates by

$$r = a(1 + g(\theta)), \quad (2)$$

where the deviation  $g(\theta)$  is expressed in terms of the Legendre polynomials as

$$g(\theta) = \sum_{l=1}^{\infty} g_{2l} P_{2l}(\cos \theta). \quad (3)$$

The coefficients,  $g$ 's, are assumed to be small and the perturbation method will be used in the following discussions.

The electric potentials  $\phi_e$  and  $\phi_i$  were determined in I for a conducting membrane. It can be shown that the potential  $\phi_e$  for an insulating membrane is derived from  $\phi_e$  for a conducting membrane by setting  $\sigma_i = 0$ . The result is

$$\phi_e = -a_0 E_0 \left[ \left( \frac{r}{a_0} + \frac{a_0^2}{2r^2} \right) \cos \theta + \sum_{l=1}^{\infty} \left( \frac{a_0}{r} \right)^{2l+1} C_{2l+1} P_{2l+1}(\cos \theta) \right], \quad (4)$$

where

$$C_{2l+1} = \frac{3}{2} (2l+1) \left[ \frac{g_{2l}}{4l+1} - \frac{g_{2l+2}}{4l+5} \right]. \quad (5)$$

The normal component of the force acting on the vesicle can be derived from eqs. (1) and (4), and is given by

\*These boundary conditions are also given by eq. (2.4) of I. However, it contains typographical errors.  $\sigma$ 's should appear in the expression for the boundary conditions of normal components as given herein.

$$F_n = -\frac{9}{32\pi} \epsilon_e E_0^2 \sin^2 \theta \left[ 1 - 2g(\theta) + \frac{4}{3} \sum_{l=0}^{\infty} C_{2l+1} \frac{dP_{2l+1}(\cos \theta)}{d \cos \theta} \right] + O(g^2). \quad (6)$$

The leading term of this equation is identical to the expression derived by Helfrich and always produces a prolate deformation of a vesicle.

### 2.3 Model of dynamics

In I, equations of membrane motion have been constructed from the Lagrangean consisting of the inertial as well as curvature elastic energy terms. The equations also involve the electric force and the force due to the resistance of the surrounding fluid. They are reduced to linear coupled equations given as

$$\ddot{g}_2 + 2\Gamma\dot{g}_2 + D_2 g_2 = 2G \quad (7)$$

$$\ddot{g}_4 + 2\Gamma\dot{g}_4 + D_4 g_4 = \frac{216}{35} G g_2, \quad (8)$$

where  $D_2$ ,  $D_4$  and  $G$  are given by

$$D_2 = K_2 + \frac{61}{35} K_E \quad (9)$$

$$D_4 = K_4 + \frac{81}{77} K_E \quad (10)$$

$$G = \frac{1}{4} K_E \quad (11)$$

for an insulating membrane.  $\Gamma$ ,  $K_E$ ,  $K_2$  and  $K_4$  are defined in I and depend on the field strength  $E_0$ , the vesicle radius  $a_0$  and the dielectric constant of the fluid outside the vesicle. They also contain the fluid resistance coefficient,  $\gamma$ , the mass factor,  $\nu$ , and the curvature elastic modulus,  $\kappa$ . In the case of a conducting membrane, similar expressions for  $D_2$ ,  $D_4$  and  $G$  are given in I.

If the applied field is switched off, the dynamical equations are given by eqs. (8) and (9) with  $D_2 = K_2$ ,  $D_4 = K_4$  and  $G = 0$ .  $D_2$ ,  $D_4$  and  $G$  for a conducting membrane depend on the ratio  $x = \sigma_i / \sigma_e$ . It was shown that the driving force term,  $G$ , is positive (negative) for  $x > 1$  ( $x < 1$ ). The sign of  $G$  determines the mode of deformation; prolate if  $G > 0$  and oblate if  $G < 0$ . In contrast,  $G$  for an insulating membrane is always positive as can be seen from eq. (11). Thus, the deformation is always prolate as pointed out by Helfrich.<sup>6)</sup>

It should be noted from eqs. (9) and (10) that the electric field gives positive contributions to the restoring force constants. On the other hand, it was shown in I that the electric field may give negative contributions for certain values of  $x$ .

### §3. Calculations

In a typical experiment, a pulsed field with the duration of  $t_0$  is applied and the time dependence of the deformation is measured.<sup>1)</sup> If the field is strong enough, the electro-poration occurs at  $t = t_p$  ( $< t_0$ ). After the field is switched off, the deformation continues to increase, reaching a maximum at  $t = t_{\max}$ , and it decreases nearly exponentially to zero with the time constant  $t_r$ . The expres-

sion for  $t_{\max}$  in terms of  $g_2(t_0)$  and  $g_2(t_0)$  is given in I. For a certain ranges of  $x$  and  $t_p$ ,  $g_2$  reaches a maximum only before the electric field is turned off and it decreases to zero monotonically thereafter. In such cases,  $t_{\max}$  does not exist.

Calculations have been carried out for a typical set of values of  $E_0 = 500 \text{ Vcm}^{-1}$ ,  $t_0 = 500 \mu\text{s}$  and  $a_0 = 10 \mu\text{m}$ . The values of the parameters,  $\nu$  and  $\kappa$  were the same as those used in I. The fluid resistance coefficient,  $\gamma$ , was set to  $7.5 \text{ gcm}^{-2}\text{s}^{-1}$  as in I. For this set of parameters,  $t_r/t_0 = 21.5$ . Figure 1 shows the time evolution of  $g_2$  and  $g_4$  for  $x=2$ . Calculations were performed for  $t_p/t_0 = 0, 0.5$  and 1. The value of  $t_{\max}$  was found nearly independent of  $t_p$ . The ratio  $t_{\max}/t_0$  ranges from 3.58 for  $t_p/t_0 = 0$  to 3.45 for  $t_p/t_0 = 1$ . It can be seen that the overall behavior is essentially the same for different  $t_p$ . The maximum deformation is attained for  $t_p/t_0 \approx 0.5$  in this case. It can be shown that the driving force term,  $G$ , for a conducting membrane coincides with that for an insulating membrane if  $x = 2/3(1 + \sqrt{7}) = 2.43$ . Since eq. (8) gives  $g_2 = Gt^2 + O(t^3)$  for small values of  $t$ , the initial behavior is the same irrespective of whether the membrane is conducting or non-conducting. Figure 2 shows the time dependences of  $g_2$  and  $g_4$  for  $x=2.43$  with  $t_p/t_0 = 0, 0.5$  and 1. The difference in the time dependence for larger values of  $t$  is due to the difference between the restoring force  $D_2$  for the conducting membrane and that for the non-conducting membrane.  $D_2$  for a conducting membrane in a strong field can be very small and even be negative in contrast to  $D_2$  given by eq. (9) for a non-conducting membrane.

The results of calculations for  $x=0.2$  are depicted in Fig. 3. The time evolution is strongly dependent on  $t_p/t_0$  contrary to that for  $x > 1$ . Since the deformation of a conducting membrane is oblate for  $x < 1$ ,  $g_2$  remains negative

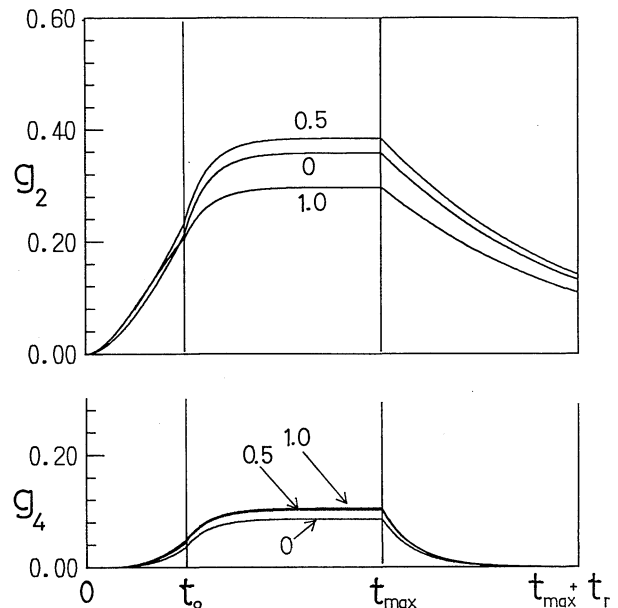


Fig. 1. Time evolution of  $g_2$  and  $g_4$  calculated for  $x=2$ . Calculations were made for  $t_p/t_0 = 0, 0.5$  and 1. The numbers in the figure represent the values of  $t_p/t_0$ . Note that the linear scales for the regions  $0 < t < t_0$ ,  $t_0 < t < t_{\max}$  and  $t_{\max} < t < t_{\max} + t_r$  are different. The values of  $t_{\max}/t_0$  and  $t_r/t_0$  are given in the text.

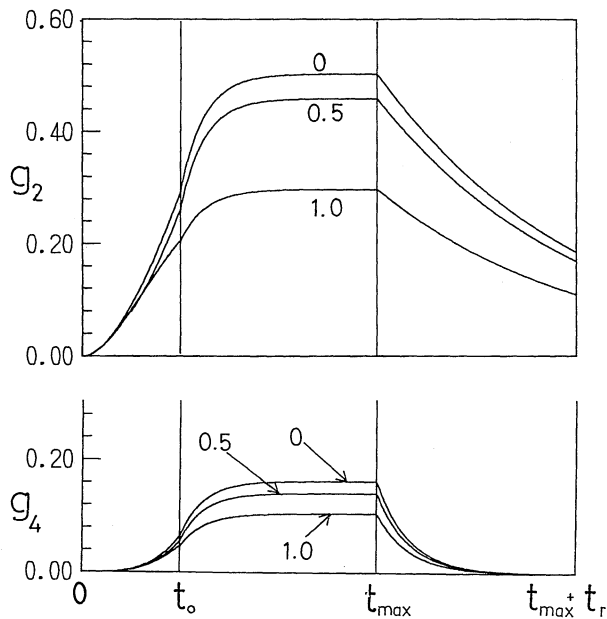


Fig. 2. Time evolution of  $g_2$  and  $g_4$  calculated for  $x=2.43$ . Calculations were made for  $t_p/t_0=0, 0.5$  and  $1$ . The numbers in the figure represent the values of  $t_p/t_0$ . Note that the linear scales for the regions  $0 < t < t_0$ ,  $t_0 < t < t_{\max}$  and  $t_{\max} < t < t_{\max} + t_r$  are different. The values of  $t_{\max}/t_0$  and  $t_r/t_0$  are given in the text.

for  $t_p=0$  as concluded in I. For  $t_p \neq 0$ ,  $g_2$  always increases initially. However, if  $t_p$  is small the dynamics is overwhelmed by that for a conducting membrane and the deformation eventually becomes oblate. For  $0 < t_p/t_0 < 0.46$ ,  $g_2$  becomes eventually negative and thus has two extrema, the one at  $t < t_0$  and the other at  $t = t_{\max} > t_0$ .  $t_{\max}/t_0$  for  $t_p/t_0=0$  and  $0.25$  are  $3.56$  and  $3.82$ , respectively. For  $t_p/t_0 > 0.74$ ,  $g_2$  continues to increase after  $t_p$  and reaches a maximum at  $t = t_{\max} > t_0$ . The ratio  $t_{\max}/t_0$  for  $t_p/t_0=0.75$  and  $1$  are  $2.02$  and  $3.45$ , respectively. For  $0.46 < t_0 < 0.74$ ,  $g_2$  reaches a maximum value at a certain  $t < t_0$  and then decreases monotonically to zero. In this case,  $t_{\max}$  does not exist as pointed out above. In Fig. 3, the result of calculation for  $t_p/t_0=0.5$  is presented with  $t_{\max}/t_0$  set arbitrarily to  $4$ .

#### §4. Conclusion

In the present model the motion of the fluid surrounding the membrane is assumed to be describable in terms of the mass factor,  $\nu$ , and the fluid resistance coefficient,  $\gamma$ . In order to go beyond this model, one needs to use the hydrodynamic equation of the fluid. However, even the

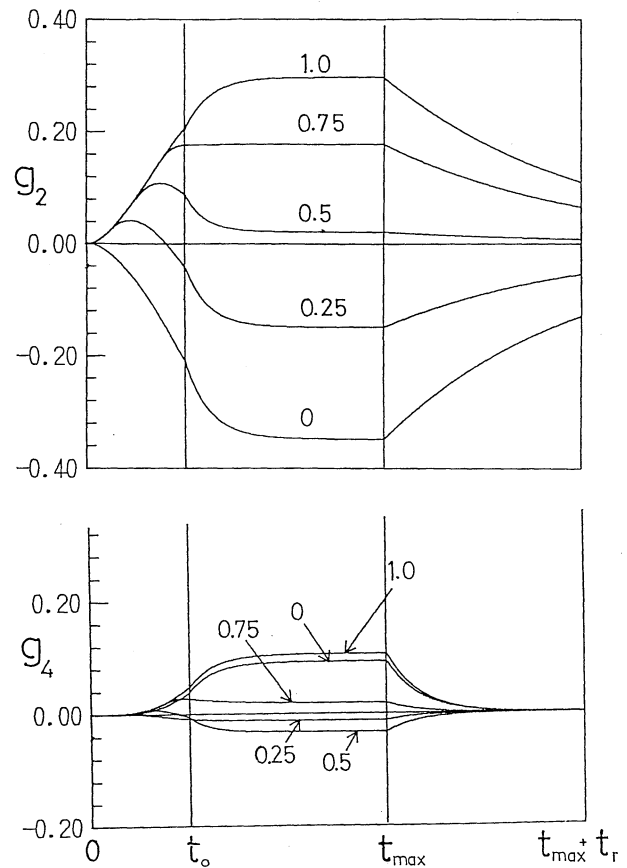


Fig. 3. Time evolution of  $g_2$  and  $g_4$  calculated for  $x=0.2$ . Calculations were made for  $t_p/t_0=0, 0.5$  and  $1$ . The numbers in the figure represent the values of  $t_p/t_0$ . Note that the linear scales for the regions  $0 < t < t_0$ ,  $t_0 < t < t_{\max}$  and  $t_{\max} < t < t_{\max} + t_r$  are different. The values of  $t_{\max}/t_0$  and  $t_r/t_0$  are given in the text.

simplified model used in the present calculations appears to give reasonable description of the dynamics of the vesicle deformation, and it may be useful in analyzing experimental data obtained in the field of electroporation of cells.

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